

RUN

Berechnung 'SCHUB' B. Zindler Ø8.04.1994

a = 2
b = 2
 $e(y) = 1$
 $e(z) = 1$

| Alpha | $F(\tau)n$ | Ω | Ω' |
|-------|------------|----------|-----------|
| Ø | 35.3 | 5Ø | 5Ø |
| 5 | 38.3 | 54 | 54 |
| 10 | 4Ø.9 | 58 | 58 |
| 15 | 43.3 | 61 | 61 |
| 20 | 45.3 | 64 | 64 |
| 25 | 46.9 | 65 | 66 |
| 30 | 48.2 | 68 | 68 |
| 35 | 49.2 | 7Ø | 7Ø |
| 40 | 49.8 | 7Ø | 7Ø |
| 45 | 5Ø | 71 | 71 |
| 50 | 49.8 | 7Ø | 7Ø |
| 55 | 49.2 | 7Ø | 7Ø |
| 60 | 48.2 | 68 | 68 |
| 65 | 46.9 | 66 | 66 |
| 70 | 45.3 | 64 | 64 |
| 75 | 43.3 | 61 | 61 |
| 80 | 4Ø.9 | 58 | 58 |
| 85 | 38.3 | 54 | 54 |
| 90 | 35.3 | 5Ø | 5Ø |

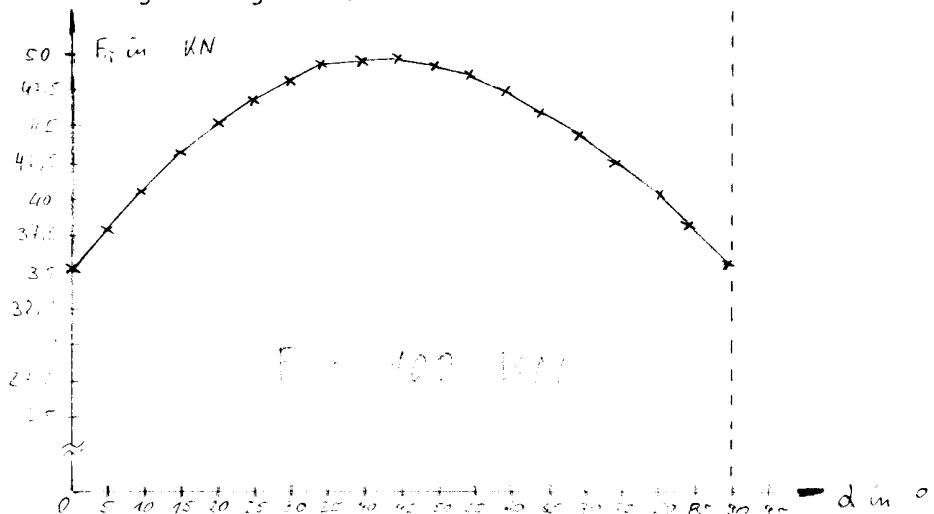
Beta = 45
Delta= 45

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

Alpha, Beta, Gamma in Grad(Alt) '°'
 $F(\tau)n$, Ω , Ω' in Kilonewton 'KN'
a, b, $e(y)$, $e(z)$ in Meter 'm'

Es folgt Diagramm.



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RUN

Berechnung 'SCHUB' B. Zindler Ø3.04.1994

a = 2
b = 3
 $e(y) = .5$
 $e(z) = .5$

| Alpha | $F(\tau)n$ | Ω | Ω' |
|-------|------------|----------|-----------|
| Ø | 15 | 25 | 17 |
| 5 | 16.2 | 27 | 18 |
| 10 | 17.4 | 29 | 19 |
| 15 | 18.3 | 31 | 20 |
| 20 | 19.2 | 32 | 21 |
| 25 | 19.9 | 33 | 22 |
| 30 | 20.5 | 34 | 23 |
| 35 | 20.9 | 35 | 23 |
| 40 | 21.1 | 35 | 23 |
| 45 | 21.2 | 35 | 24 |
| 50 | 21.1 | 35 | 23 |
| 55 | 20.9 | 35 | 23 |
| 60 | 20.5 | 34 | 23 |
| 65 | 19.9 | 33 | 22 |
| 70 | 19.2 | 32 | 21 |
| 75 | 18.3 | 31 | 20 |
| 80 | 17.4 | 29 | 19 |
| 85 | 16.2 | 27 | 18 |
| 90 | 15 | 25 | 17 |

Beta = 56.3

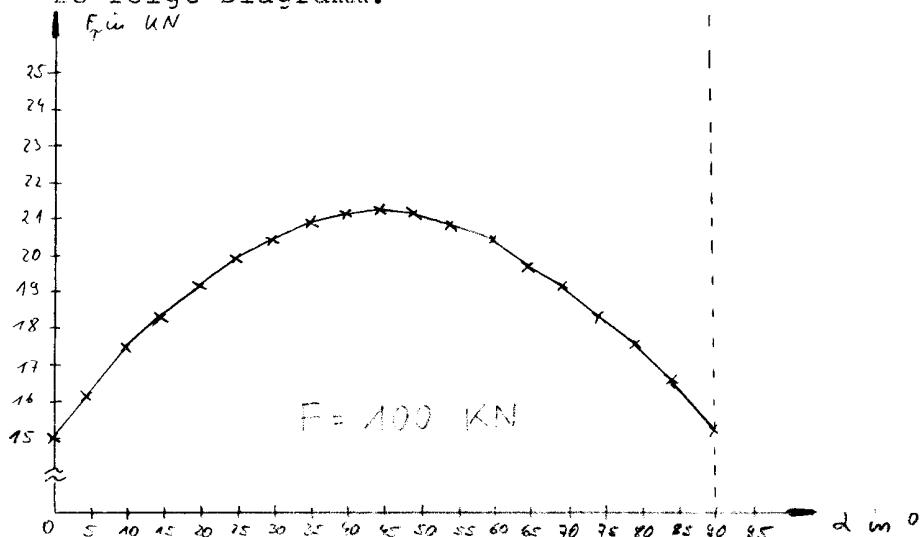
Delta = 33.6

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

Alpha, Beta, Gamma in Grad(Alt) '°'
 $F(\tau)n$, Ω , Ω' in Kilonewton 'KN'
a, b, $e(y)$, $e(z)$ in Meter 'm'

Es folgt Diagramm.



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Berechnung 'Zug' B. Zindler 09.04.1994
a = 2
b = 2
 $e(z) = b/a * e(y)$

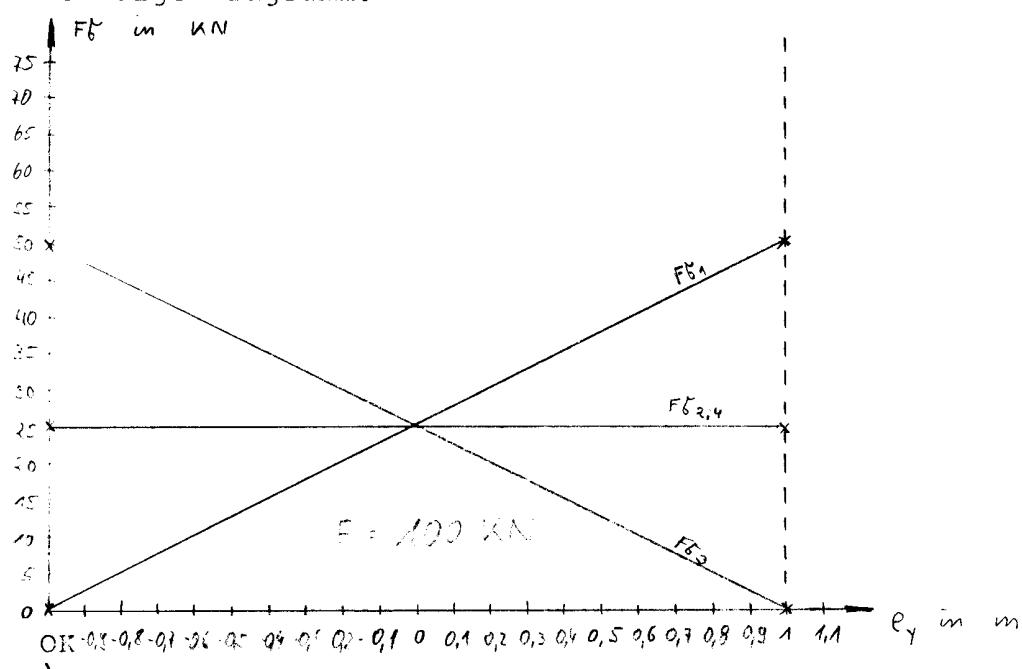
| $e(y)$ | $e(z)$ | $F(\sigma)_1;2;3;4$ | | | |
|--------|--------|---------------------|----|----|----|
| -1 | -1 | Ø | 25 | 5Ø | 25 |
| -.9 | -.9 | 3 | 25 | 48 | 25 |
| -.8 | -.8 | 5 | 25 | 45 | 25 |
| -.7 | -.7 | 8 | 25 | 43 | 25 |
| -.6 | -.6 | 1Ø | 25 | 4Ø | 25 |
| -.5 | -.5 | 13 | 25 | 38 | 25 |
| -.4 | -.4 | 15 | 25 | 35 | 25 |
| -.3 | -.3 | 18 | 25 | 33 | 25 |
| -.2 | -.2 | 2Ø | 25 | 3Ø | 25 |
| -.1 | -.1 | 23 | 25 | 28 | 25 |
| Ø | Ø | 25 | 25 | 25 | 25 |
| .1 | .1 | 28 | 25 | 23 | 25 |
| .2 | .2 | 3Ø | 25 | 2Ø | 25 |
| .3 | .3 | 33 | 25 | 18 | 25 |
| .4 | .4 | 35 | 25 | 15 | 25 |
| .5 | .5 | 38 | 25 | 13 | 25 |
| .6 | .6 | 4Ø | 25 | 1Ø | 25 |
| .7 | .7 | 43 | 25 | 8 | 25 |
| .8 | .8 | 45 | 25 | 5 | 25 |
| .9 | .9 | 48 | 25 | 3 | 25 |
| 1 | 1 | 5Ø | 25 | Ø | 25 |

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

a, b, $e(y)$, $e(z)$ in Meter 'm'
 $F(\sigma)_n$ in Kilonewton 'KN'
Sigmawerte gerundet!

Es folgt Diagramm.



RUN

Berechnung 'Zug' B. Zindler 09.04.1994
a = 2
b = 3
 $e(z) = e(y)$

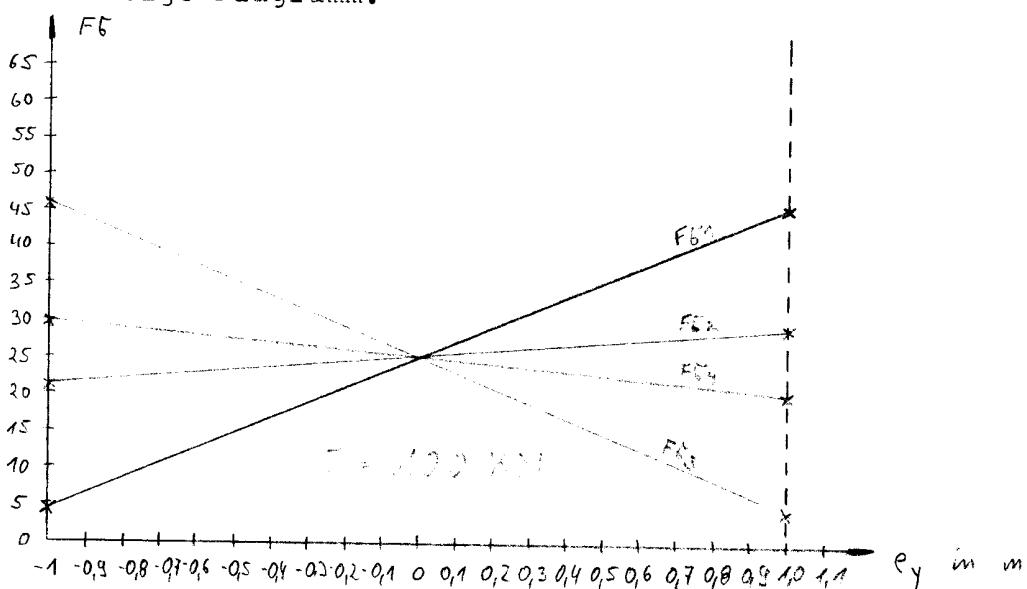
| $e(y)$ | $e(z)$ | F(sigma)1;2;3;4 | | | |
|--------|--------|-----------------|----|----|----|
| -1 | -1 | 4 | 21 | 46 | 29 |
| -.9 | -.9 | 6 | 21 | 44 | 29 |
| -.8 | -.8 | 8 | 22 | 42 | 28 |
| -.7 | -.7 | 10 | 22 | 40 | 28 |
| -.6 | -.6 | 12 | 23 | 38 | 28 |
| -.5 | -.5 | 15 | 23 | 35 | 27 |
| -.4 | -.4 | 17 | 23 | 33 | 27 |
| -.3 | -.3 | 19 | 24 | 31 | 26 |
| -.2 | -.2 | 21 | 24 | 29 | 26 |
| -.1 | -.1 | 23 | 25 | 27 | 25 |
| 0 | 0 | 25 | 25 | 25 | 25 |
| .1 | .1 | 27 | 25 | 23 | 25 |
| .2 | .2 | 29 | 26 | 21 | 24 |
| .3 | .3 | 31 | 26 | 19 | 24 |
| .4 | .4 | 33 | 27 | 17 | 23 |
| .5 | .5 | 35 | 27 | 15 | 23 |
| .6 | .6 | 38 | 28 | 12 | 23 |
| .7 | .7 | 40 | 28 | 10 | 22 |
| .8 | .8 | 42 | 28 | 8 | 22 |
| .9 | .9 | 44 | 29 | 6 | 21 |
| 1 | 1 | 46 | 29 | 4 | 21 |

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

a, b, $e(y)$, $e(z)$ in Meter 'm'
 $F(\sigma)_n$ in Kilonewton 'KN'
Sigmawerte gerundet!

Es folgt Diagramm.



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Berechnung 'dT-sig' B.Zindler 10.04.1994

E = 2,1 * 10⁵ --- Stahl
Alpha(1) = 1,0 * 10⁻⁶ --- Glas
Alpha(2) = 1,3 * 10⁻⁵ --- Stahl
d = 12

dT F(sigma)n

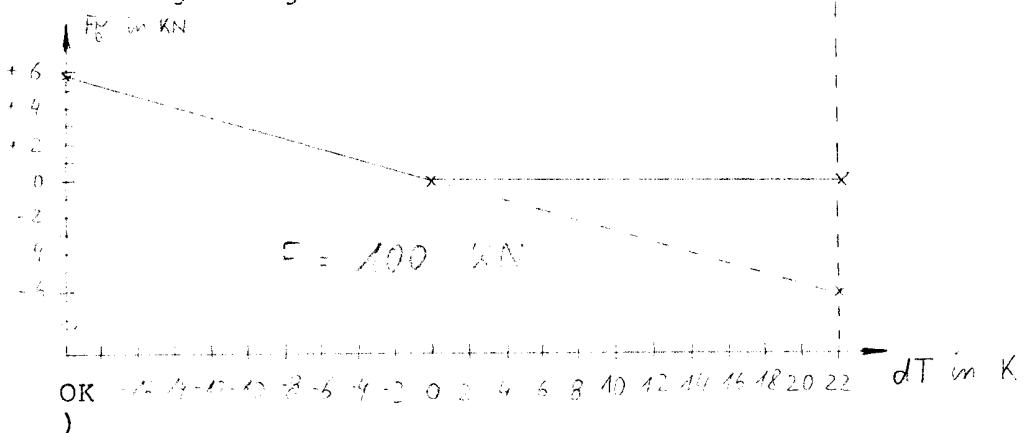
| | |
|-----|--------|
| -20 | 5.7 |
| -18 | 5.1 |
| -16 | 4.6 |
| -14 | 4 |
| -12 | 3.4 |
| -10 | 2.9 |
| -8 | 2.3 |
| -6 | 1.7 |
| -4 | 1.1 |
| -2 | .6 |
| 0 | 0 |
| 2 | 0 -.6 |
| 4 | 0 -1.1 |
| 6 | 0 -1.7 |
| 8 | 0 -2.3 |
| 10 | 0 -2.9 |
| 12 | 0 -3.4 |
| 14 | 0 -4 |
| 16 | 0 -4.6 |
| 18 | 0 -5.1 |
| 20 | 0 -5.7 |

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

E Newton je Quadratmillimeter 'Nmm,-2'
Alpha(1);(2) in Kelvin,-1 'K,-1'
d in Millimeter 'mm'
dT in Kelvin 'K'

Es folgt Diagramm.



RUN

Berechnung 'dT-sig' B.Zindler 10.04.1994

E = 2,1 * 10,5 --- Stahl
Alpha(1)= 2,3 * 10,-5 --- Alu
Alpha(2)= 1.3 * 10,-5 --- Stahl
d = 12

dT F(sigma)n

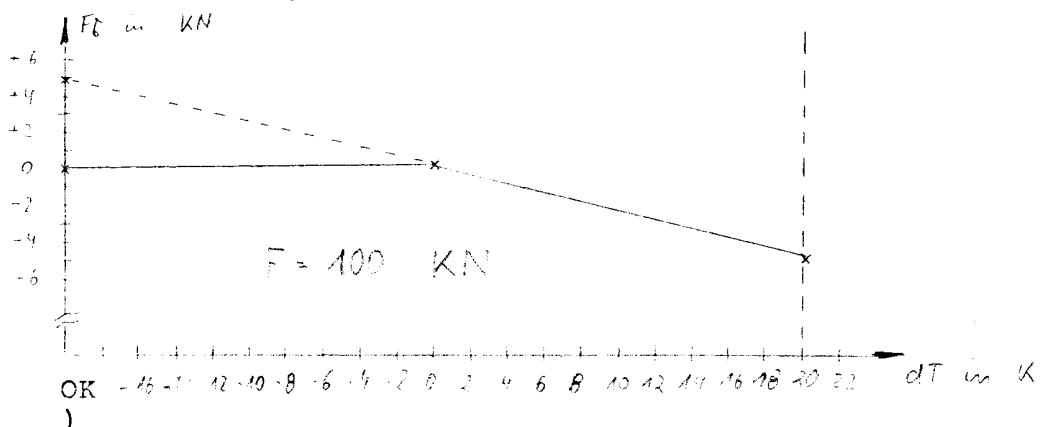
| | | |
|-----|-----|------|
| -20 | 0 | -4.8 |
| -18 | 0 | -4.3 |
| -16 | 0 | -3.8 |
| -14 | 0 | -3.3 |
| -12 | 0 | -2.9 |
| -10 | 0 | -2.4 |
| -8 | 0 | -1.9 |
| -6 | 0 | -1.4 |
| -4 | 0 | -1 |
| -2 | 0 | -.5 |
| 0 | 0 | |
| 2 | .5 | |
| 4 | 1 | |
| 6 | 1.4 | |
| 8 | 1.9 | |
| 10 | 2.4 | |
| 12 | 2.9 | |
| 14 | 3.3 | |
| 16 | 3.8 | |
| 18 | 4.3 | |
| 20 | 4.8 | |

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

E Newton je Quadratmillimeter 'Nmm,-2'
Alpha(1);(2) in Kelvin,-1 'K,-1'
d in Millimeter 'mm'
dT in Kelvin 'K'

Es folgt Diagramm.



RUN

Berechnung 'dT-sig' B.ZINDLER 10.04.1994

E = 2,1 * 10,5 --- Stahl
Alpha(1)= 1,2 * 10,-5 --- Beton B10
Alpha(2)= 1,3 * 10,-5 --- Stahl
d = 12

dT F(sigma)n

| | |
|-----|-----|
| -20 | .48 |
| -18 | .43 |
| -16 | .38 |
| -14 | .33 |
| -12 | .29 |
| -10 | .24 |
| -8 | .19 |
| -6 | .14 |
| -4 | .1 |
| -2 | .05 |
| 0 | 0 |
| 2 | 0 |
| 4 | 0 |
| 6 | 0 |
| 8 | 0 |
| 10 | 0 |
| 12 | 0 |
| 14 | 0 |
| 16 | 0 |
| 18 | 0 |
| 20 | 0 |

Alle Werte unter den gegebenen Bedingungen errechnet!

Einheiten:

E Newton in Quadratmillimeter 'Nmm,-2'
Alpha(1);(2) in Kelvin,-1 'K,-1'
d in Millimeter 'mm'
dT in Kelvin 'K'

Es folgt Diagramm.

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RUN

Berechnung 'dT-tau' B.Zindler 10.04.1994

E = 22 * 10³ --- Beton Bl⁰
Alpha = 1,2 * 10⁻⁵
t = 20
a = 2000
b = 3000
F = 100

dT F(tau)n

| | |
|-----|--------|
| -20 | 190.4 |
| -18 | 171.3 |
| -16 | 152.3 |
| -14 | 133.3 |
| -12 | 114.2 |
| -10 | 95.2 |
| -8 | 76.1 |
| -6 | 57.1 |
| -4 | 38.1 |
| -2 | 19 |
| 0 | 0 |
| 2 | -19 |
| 4 | -38.1 |
| 6 | -57.1 |
| 8 | -76.1 |
| 10 | -95.2 |
| 12 | -114.2 |
| 14 | -133.3 |
| 16 | -152.3 |
| 18 | -171.3 |
| 20 | -190.4 |

Alle Werte unter den gegebenen Randbedingungen errechnet!

Einheiten:

E Newton je Quadratmillimeter 'Nmm,-2'
Alpha in Kelvin,-1 'K,-1'
t, a, b IN Millimeter 'mm'
dT in Kelvin 'K'

Es folgt Diagramm.

